

selected with temperatures of 850°C, 875°C, and 900°C, which is cofiring compatible temperature for Ag and low temperature cofired ceramics (LTCC) substrate. Density in different sintering temperature is shown in Figure 2.

Figure 3 shows the XRD patterns of the samples sintered 900°C for 2h in PZT-PZN-PNN based compositions + x wt% CuO ceramics. It can be seen in Figure 3 that all samples exhibit a perovskite structure, and that there is no secondary phase until $x=0.2$ (any peak for secondary phase was not detected in the range of 0.0-0.2). When x was over 0.3, second phase peak was observed, however, a composition for the second peak was not clearly identified.

Figure 4 shows the SEM images of the PZT-PZN-PNN based compositions + x wt% CuO ceramics sintered at 900°C for 2h. As the CuO addition amount increased, grain growth happened whereas small grains disappeared. This grain growth with CuO addition can be explained with liquid phase sintering. Previously, we showed that the

addition of CuO can reduce the sintering temperature of the $\text{Pb}(\text{Zr},\text{Ti})\text{O}_3\text{-Pb}(\text{Ni},\text{Nb})\text{O}_3$ system by the formation of a liquid phase [13]. Thus this liquid phase formation can also be an explanation for the PZT-PZN-PNN based compositions + x wt% CuO ceramics.

Density, dielectric permittivity ($\epsilon_{33}^T/\epsilon_0$), electromechanical coupling factor (k_p), mechanical quality factor (Q_m) and piezoelectric constant (d_{33}) were plotted as a function of the amount of CuO addition in Figure 5. The density was increased with the increase of CuO contents approximately from 6.4 to 7.8 g/cm³. This improvement of the density might be related to the formation of the liquid phase. Moreover, the variation of piezoelectric and dielectric properties showed similar trend to that of density. Therefore, the improved piezoelectric and dielectric properties, which were observed in the range of $x \geq 0.3$, might be due to the increased density as well as increased grain size shown in Figure 4. This hardening effect that could be confirmed by the enhancement of Q_m value approximately from 600 to 1200 as shown in Figure 5.

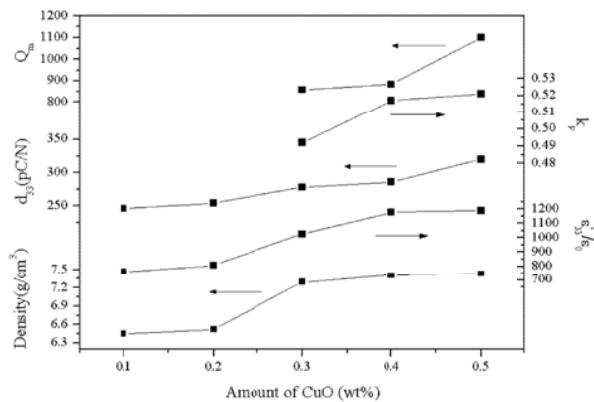


Figure 5. Density, dielectric permittivity ($\epsilon_{33}^T/\epsilon_0$), piezoelectric constant (d_{33}), electromechanical coupling factor (k_p) and mechanical quality factor (Q_m) of the specimens sintered at 900°C for 2h in PZT-PZN-PNN based compositions + x wt% CuO ceramics.

Therefore, Cu ions could be expected to enter B site and act as a hardener.

3.2 Effect of Bi_2O_3 Addition

Bi_2O_3 has low melting temperature (817°C) and it was reported that Bi_2O_3 can form liquid phase with ZnO at approximately 750°C. Therefore, Bi_2O_3 was added to PZT-PZN-PNN based compositions + 0.5 wt% CuO in order to further improve the piezoelectric properties of the specimens sintered at low temperature. Density in different sintering temperature is shown in Figure 6.

Figure 7 shows the XRD patterns of the samples sintered 900°C for 2h in PZT-PZN-PNN based compositions + 0.5 wt% CuO + y wt% Bi_2O_3 ceramics. It can be seen that all the samples exhibit a perovskite structure. The base composition (y=0) had a slight tetragonal symmetry. The tetragonality of the peaks was reduced until y=0.3; but it was

increased when the amount of Bi_2O_3 addition exceeded 0.3 wt%.

Figure 8 shows the SEM images of the PZT-PZN-PNN based compositions + 0.5 wt% CuO + y wt% Bi_2O_3 ceramics sintered at 900°C for 2 h. When the amount of Bi_2O_3 was more than 0.3 wt%, the small grains almost disappeared and average grain size increased. Even though apparent liquid phase formation was not observed in the SEM images, Bi_2O_3 addition might induce small amount of liquid phase and it could be expected to help grain growth due to its low melting point.

Density, dielectric permittivity ($\epsilon_{33}^T/\epsilon_0$), electromechanical coupling factor (k_p), mechanical quality factor (Q) and piezoelectric constant (d_{33}) of PZT-PZN-PNN based compositions + 0.5 wt% CuO + y wt% Bi_2O_3 ceramics sintered at 900°C for 2 h are plotted as a function of the amount of Bi_2O_3 addition

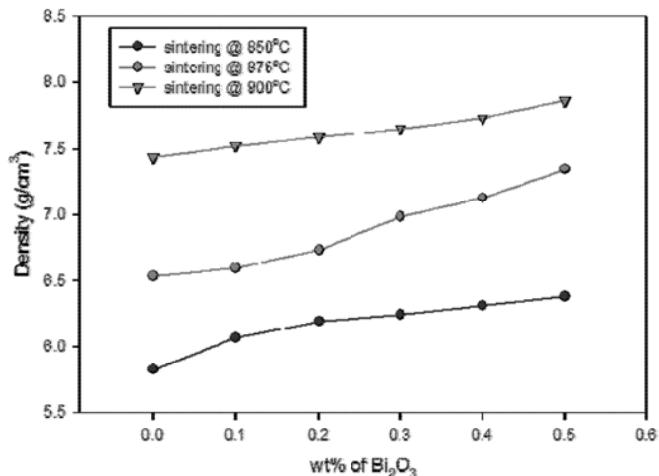


Figure 6. Density in different sintering temperature in PZT-PZN-PNN based compositions + 0.5 wt% CuO + y wt% Bi_2O_3 ceramics.

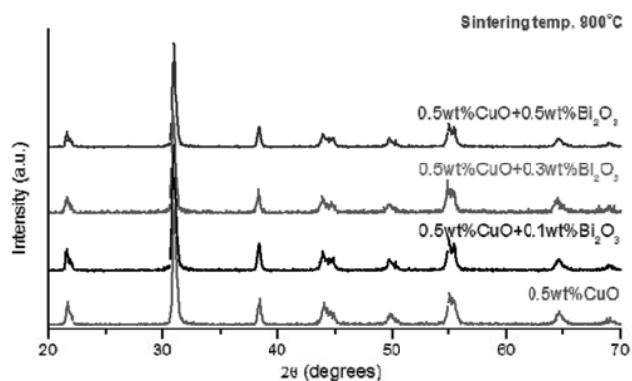


Figure 7. XRD patterns of the samples sintered 900°C for 2h in PZT-PZN-PNN based compositions + 0.5 wt% CuO + y wt% Bi₂O₃ ceramics.

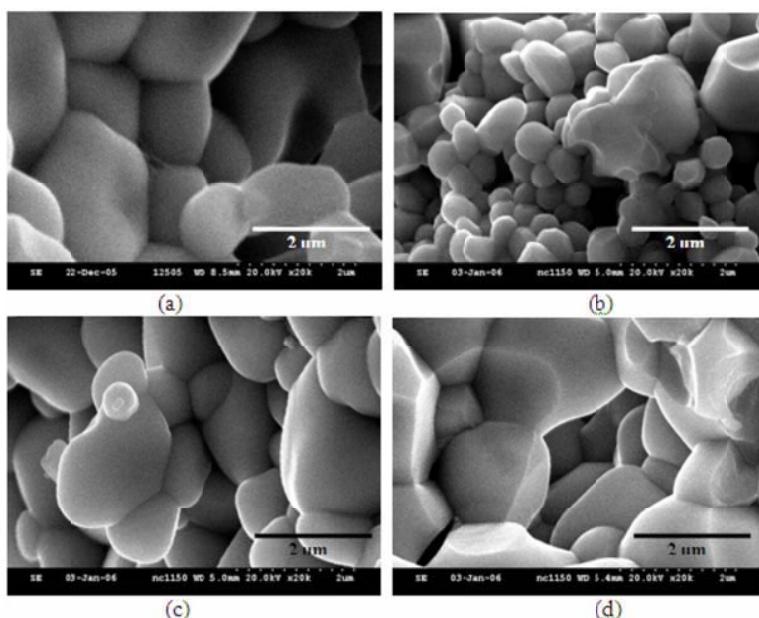


Figure 8. SEM images of the samples sintered at 900°C for 2h in PZT-PZN-PNN based compositions + 0.5 wt% CuO + y wt% Bi₂O₃ ceramics : (a) y=0, (b) y=0.1, (c) y=0.3 and (d) y=0.5.

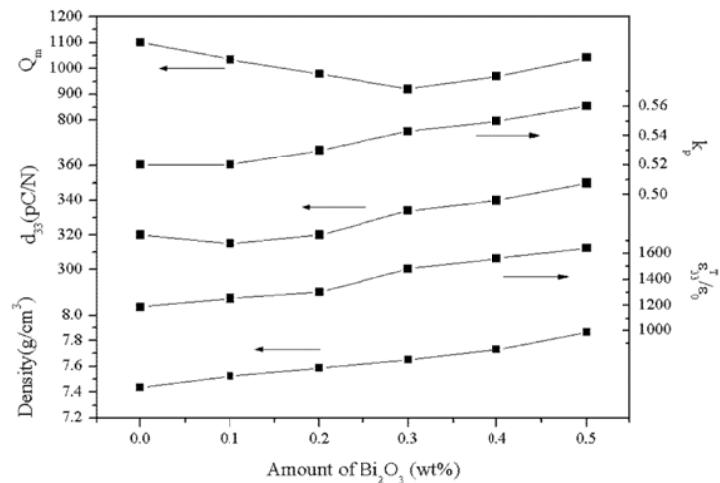


Figure 9. Density, dielectric permittivity ($\epsilon_{33}^T/\epsilon_0$), piezoelectric constant (d_{33}), electromechanical coupling factor (k_p) and mechanical quality factor (Q_m) of the specimens sintered at 900°C for 2h in PZT-PZN-PNN based compositions + 0.5 wt% CuO + y wt% Bi_2O_3 ceramics.

in Figure 9. When Bi_2O_3 was added, density was increased and this increased density improved the dielectric and piezoelectric properties as seen in Figure 8. The density of the specimens was improved when the amount of Bi_2O_3 was added and this increase might be due to the formation of liquid phase. In addition, Q_m was decreased and $\epsilon_{33}^T/\epsilon_0$ and d_{33} were increased with the amount of Bi_2O_3 addition in the range of $0.0 \leq y \leq 0.3$. Therefore, their variations could happen because Bi ions entered A site, since they acted as softener in this range. On the contrary, Q_m exhibits a minimum profile at 0.3 wt% of Bi_2O_3 addition. In addition, $\epsilon_{33}^T/\epsilon_0$, d_{33} and Q_m were increased with the amount of Bi_2O_3 addition above 0.3 wt%. Thus, Bi ions might act as both hardener and softener in this range and their variations might be able to occur because Bi ions entered B site and A site, respectively.

4. CONCLUSIONS

The addition of CuO decreases the sintering temperature through the formation of a liquid phase. However, the piezoelectric properties of the CuO-added ceramics sintered at below 900°C are lower than the desired values. The additional Bi_2O_3 results in a significant improvement in the piezoelectric properties. Furthermore, at the sintering temperature of 900°C, the electromechanical coupling factor (k_p), piezoelectric constant (d_{33}), mechanical quality factor (Q_m) of PZT-PZN based composition ceramics with 0.5 wt% CuO and 0.5 wt% Bi_2O_3 show the optimal value of 0.56, 350 pC/N and 1042, respectively.

5. ACKNOWLEDGEMENTS

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Effect of MnO_2 Addition on Dielectric, Piezoelectric and Ferroelectric Properties of $0.2\text{Pb}(\text{Zn}_{1/3}\text{Nb}_{2/3})\text{O}_3-0.8\text{Pb}(\text{Zr}_{1/2}\text{Ti}_{1/2})\text{O}_3$ Ceramics

Athipong Ngamjaruojana, and Supon Ananta*

Department of Physics, Faculty of Science, Chiang Mai University, Chiang Mai 50200, Thailand.

*Author for correspondence; e-mail: suponananta@yahoo.com

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ABSTRACT

Piezoelectric materials are presently being extensively developed for applications such as ultrasonic motors and piezoelectric transformers. In this study, the dielectric, piezoelectric, and ferroelectric properties of MnO_2 -doped $0.2\text{Pb}(\text{Zn}_{1/3}\text{Nb}_{2/3})\text{O}_3-0.8\text{Pb}(\text{Zr}_{1/2}\text{Ti}_{1/2})\text{O}_3$ (hereafter 0.2PZN-0.8PZT), which is the morphotropic phase boundary composition of the PZN-PZT system, were investigated. It was found that crystal structure moved to rhombohedral side when increasing MnO_2 content. With the addition of MnO_2 , Curie temperature T_c , the piezoelectric constant d_{33} , and electromechanical coupling factor k_p were slightly decreased, but the mechanical quality factor Q_m was significantly increased. The $P-E$ and $s-E$ loop demonstrated decreased P_e and strain level but increased E_e with addition of MnO_2 . These results clearly showed the significance of MnO_2 addition on the electrical properties of the PZN-PZT system with "hard" characteristics.

Keywords: dielectric, piezoelectric, ferroelectric, hard doping.

1. INTRODUCTION

All commercial piezoelectric devices employ $\text{Pb}(\text{Zr},\text{Ti})\text{O}_3$ (PZT)-based formulations, close to the morphotropic phase boundary (MPB). The MPB composition is modified by the acceptor and/or donor ions to yield high piezoelectric properties with low losses. The influence of various substitutions on the B-site of $\text{Pb}(\text{Zr},\text{Ti})\text{O}_3$ perovskite has been widely investigated to optimize the piezoelectric properties [1-6]. Fan and Kim [7] investigated $\text{Pb}(\text{Zn}_{1/3}\text{Nb}_{2/3})_{0.5}(\text{Zr}_{0.4}\text{Ti}_{0.5})_{0.5}\text{O}_3$ ceramics with composition close to MPB and clarified that the ceramics had large electro-mechanical coupling factor k_p .

However, the mechanical quality factor Q_m was too low to permit their use as high power piezoelectric devices. It is necessary to improve Q_m as much as possible for suppressing the generation of heat during operation. To develop materials suitable for multilayer piezoelectric transformers and actuators with high d_{33} , high k_p and Q_m , it is necessary to add some dopants to PZN-PZT based ceramics to optimize the piezoelectric properties for device applications [8-11].

Manganese ions have been investigated extensively as effective dopant in PZT-based ceramics because Mn ions can have valence

3. RESULTS AND DISCUSSION

Perovskite phase formation, crystal structure and lattice parameter were determined by XRD at room temperature. The XRD patterns of 0.2Pb(Zn_{1/3}Nb_{2/3})O₃-0.8Pb(Zr_{1/2}Ti_{1/2})O₃ with the addition of 0.0-0.9 wt% MnO₂ are shown in Figure 1, showing the perovskite structure for all compositions. The pyrochlore phase is not observed in this system. In the XRD patterns, the crystal structure of the specimens appears clearly to change to rhombohedral side across MPB with increasing amount of MnO₂ around 0.5 wt%. It has been reported [6,8] that manganese coexists mainly in the Mn²⁺ and Mn³⁺ states, which entered into the perovskite structure of BO₆ octahedron to substitute for the B-site ion (e.g., Ti⁴⁺ and Zr⁴⁺).

Figure 2 shows SEM photographs of the surfaces of 0.2Pb(Zn_{1/3}Nb_{2/3})O₃-0.8Pb(Zr_{1/2}Ti_{1/2})O₃ ceramics doped with 0.0-0.9 wt% MnO₂. As shown in Figs. 2(a-b), the grain sizes of the ceramics are increased with increasing amount of MnO₂ addition. The result is similar to the result of Yu *et al.* [16]. Further increasing MnO₂ content gives rise to an inhomogeneous grain size. However, the SEM micrographs in Figure 2(c-f) show that a higher porosity level is observed when the amount of MnO₂ is increased [17]. The above results are obviously consistent with the

change in the bulk density with MnO₂ content for Mn-doped 0.2Pb(Zn_{1/3}Nb_{2/3})O₃-0.8Pb(Zr_{1/2}Ti_{1/2})O₃ ceramics. It can clearly be seen from Figure 2 that the ceramics have high densities in the MnO₂ addition range of 0.0-0.5 wt%. It is believed that manganese ions are mainly incorporated into the lattice, but if the addition is above 0.5 wt%, manganese ions will accumulate at the grain boundaries [14]. These inferences are obviously consistent with the changes mentioned above in the microstructures. The micrographs also show that the grain size of the ceramics varies considerably, as listed in Table 1.

The temperature and frequency dependences of the dielectric constant (ϵ_r) and dielectric loss tangent ($\tan \delta$) for 0.2PZN-0.8PZT + x wt% MnO₂, $x = 0, 0.1, 0.3, 0.5, 0.7$ and 0.9 are shown in Figure 3. The maximum dielectric constant at 1 kHz (ϵ_m @ 1 kHz) is listed in Table 2. Dielectric behaviors show strong increase of frequency-dependence on dielectric constant and dielectric loss with increasing amount of MnO₂. It may be caused from oxygen vacancies and conducting regions near grain boundaries [18] when increasing MnO₂. The variation of the Curie temperature (T_c) as a function of composition x is plotted in Figure 4. The Curie temperature of 0.2PZN-0.8PZT + x wt% MnO₂ system can be varied over a wide range

Table 1. Physical properties of 0.2PZN-0.8PZT + x wt% MnO₂ ceramics.

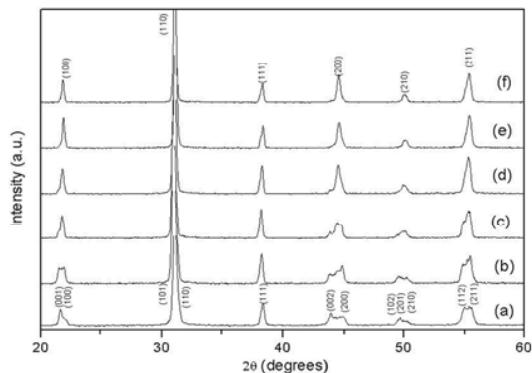
x	Density (g/cm ³)	Grain size range(μm)	Average grain size (μm)
0	7.826	0.5 - 2.0	1.726
0.1	7.849	1.5 - 6.0	4.131
0.3	7.897	1.0 - 3.0	2.991
0.5	8.028	0.5 - 2.0	2.116
0.7	7.718	-	-
0.9	7.653	-	-

Table 2. Dielectric and piezoelectric properties of 0.2PZN–0.8PZT + x wt% MnO₂ ceramics.

x	T_c (°C)	Dielectric properties (at 25 °C, 1 kHz)		Dielectric properties (at T_{Max})		Piezoelectric properties		
		ϵ_r	$\tan\delta$	ϵ_r	$\tan\delta$	d_{33} (pC/N)	k_p	Q_m
0	339.7	1575	0.0249	21047	0.0420	430	0.583	90
0.1	334.2	1155	0.0436	17784	0.1181	365	0.564	356
0.3	326.5	1100	0.0464	19102	0.1241	320	0.551	735
0.5	323.4	1086	0.0440	18220	0.1454	305	0.532	1413
0.7	318.7	1020	0.0368	21178	0.1354	263	0.48	1260
0.9	311	948	0.0438	21389	0.1762	237	0.44	1080

Table 3. Ferroelectric and strain properties of 0.2PZN–0.8PZT + x wt% MnO₂ ceramics.

x	Ferroelectric properties (at 25 °C)			Loop squareness (R_{sq})	Strain %@ 4MV/m
	P_r (C/m ²)	P_s (C/m ²)	E_C (MV/m)		
0	0.287	0.300	1.97	1.483	0.278
0.1	0.224	0.233	2.18	1.488	0.231
0.3	0.208	0.213	2.37	1.712	0.188
0.5	0.147	0.175	1.94	1.024	0.162
0.7	0.089	0.126	1.63	0.811	0.134
0.9	0.077	0.111	1.75	0.811	0.115

**Figure 1.** XRD patterns of the samples sintered at 1200°C for 2h of 0.2PZN–0.8PZT + x wt% MnO₂ ceramics: (a) $x=0$, (b) $x=0.1$, (c) $x=0.3$, (d) $x=0.5$, (e) $x=0.7$ and (f) $x=0.9$.

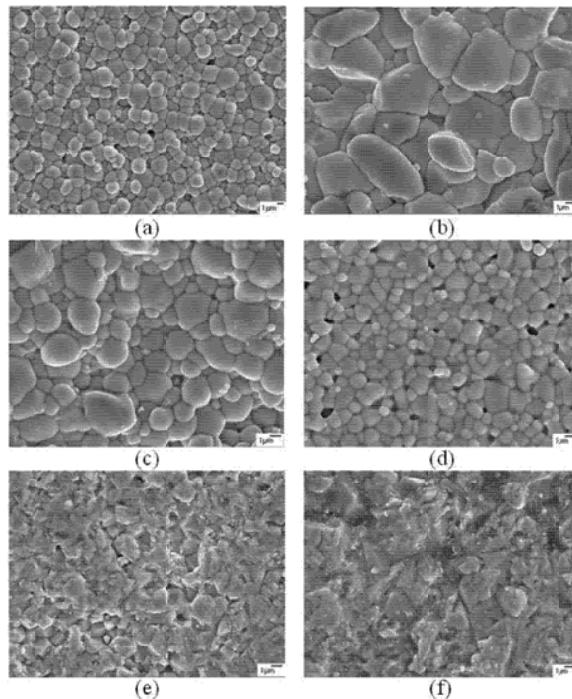


Figure 2. SEM images of the specimens sintered surface of 0.2PZN–0.8PZT+ x wt% MnO_2 ceramics at 1200°C for 2h; (a) $x=0$, (b) $x=0.1$, (c) $x=0.3$, (d) $x=0.5$, (e) $x=0.7$ and (f) $x=0.9$.

from 310 to 340 °C by controlling the addition of MnO_2 content in the system. The results indicate a rapid decrease in T_g with an increase in MnO_2 content over the range from 0.0 to 0.9 wt%.

Density, dielectric constant (ϵ_r), electro-mechanical coupling factor (k_p), mechanical quality factor and piezoelectric constant (d_{33}) are plotted as a function of amount of MnO_2 addition in Figure 5. When the amount of MnO_2 is lower than 0.5 wt%, density slightly increases. However, ϵ_r , k_p and d_{33} show decreasing trends with increasing MnO_2 content. When the amount of MnO_2 is lower than 0.5 wt%, k_p and d_{33} are rapidly decreased

with increasing MnO_2 content. It is well known that the substitutions of acceptor dopant Mn ions will lead to the creation of oxygen vacancies, which pin the movement of the ferroelectric domain walls and result in a decrease of ϵ_r , k_p and d_{33} [11,19]. The mechanical quality factor (Q_m) increases rapidly with increasing MnO_2 content [4]. The acceptor dopant of MnO_2 improves Q_m significantly. The highest value Q_m (~ 1413) are obtained in the ceramics with MnO_2 amounts of 0.5 wt%. Further addition of MnO_2 above 0.5 wt% leads to a slightly decrease in the value of Q_m , which may be mainly attributable to non-uniformity of the

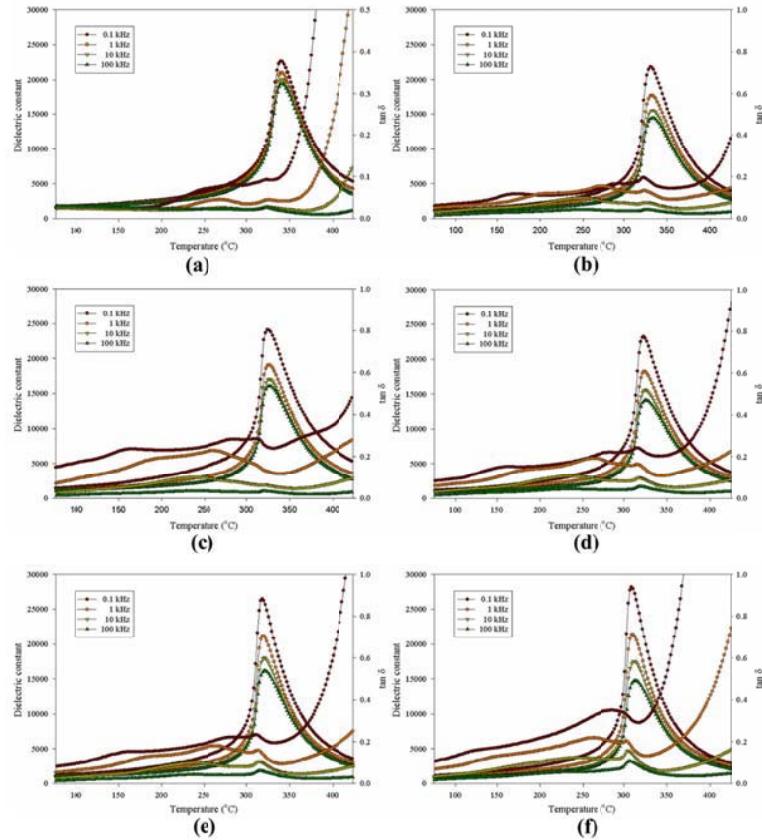


Figure 3. Temperature and frequency dependence of dielectric properties of 0.2PZN–0.8PZT + x wt% MnO_2 ceramics at 1200°C for 2h; (a) $x=0$, (b) $x=0.1$, (c) $x=0.3$, (d) $x=0.5$, (e) $x=0.7$ and (f) $x=0.9$.

microstructure, as shown in Figure 2.

The polarization-field (P – E) hysteresis loops of 0.2PZN–0.8PZT + x wt% MnO_2 ceramics are shown in Figure 6. The well-developed and fairly symmetric hysteresis loops with the field are observed for all compositions. To further assess ferroelectric

characteristics in MnO_2 -modified PZN-PZT ceramics, the ferroelectric parameters, i.e. the remnant polarization (P_r) and the coercive field (E_c), have been extracted from the experimental data and given in Table 3. It can be seen that P_r and P_s decrease with an addition of MnO_2 into the PZN-PZT

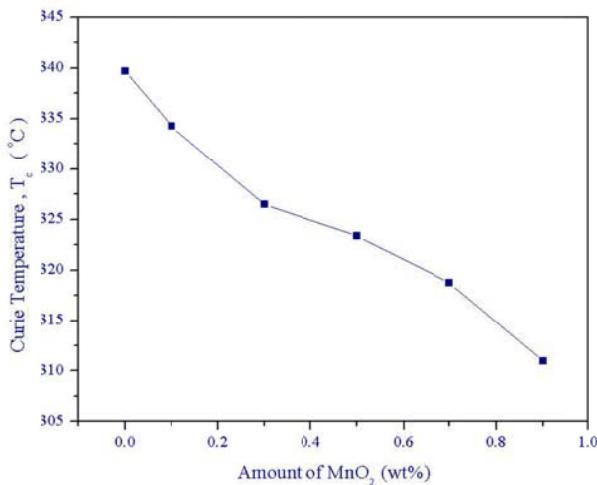


Figure 4. Curie temperature of the specimens sintered at 1200°C for 2h of 0.2PZN–0.8PZT + α wt% MnO₂ ceramics where $\alpha = 0, 0.1, 0.3, 0.5, 0.7$ and 0.9 .

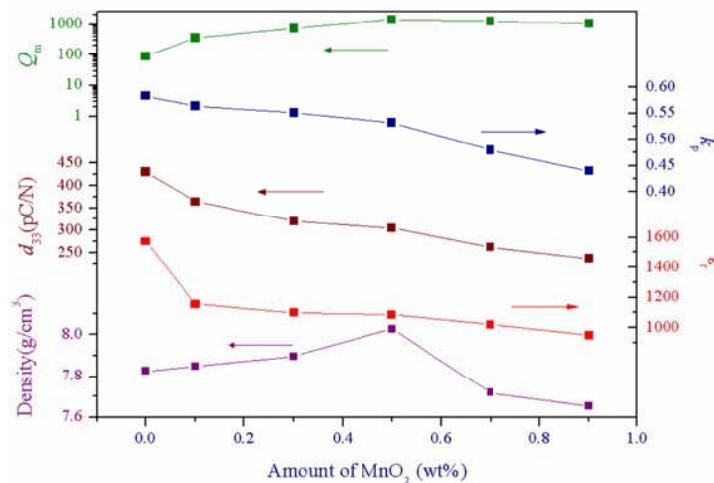


Figure 5. Density, dielectric constant (ϵ), piezoelectric constant (d_{33}), electromechanical coupling factor (k_p), and mechanical quality factor (Q_m) of the specimens sintered at 1200°C for 2h of 0.2PZN–0.8PZT + α wt% MnO₂ ceramics where $\alpha = 0, 0.1, 0.3, 0.5, 0.7$ and 0.9 .

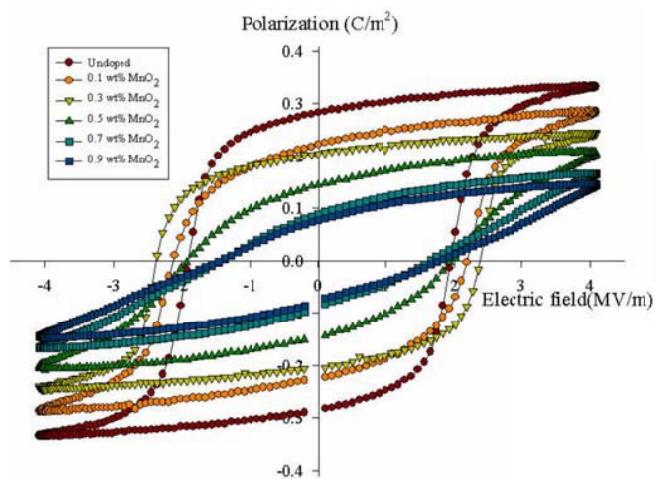


Figure 6. Polarization and electric field (P-E) loops of 0.2PZN-0.8PZT + x wt% MnO_2 ceramics.

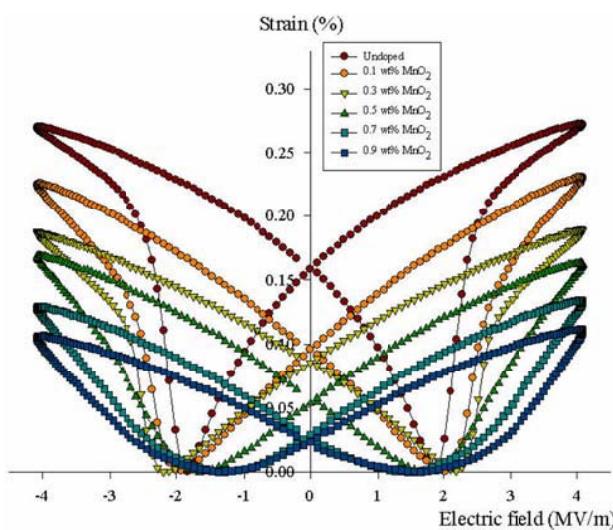


Figure 7. Strain and electric field (s-E) loops of 0.2PZN-0.8PZT + x wt% MnO_2 ceramics.

composition, while E_c increases to the maximum at $x = 0.3$ wt%. The ferroelectric characteristics can also be assessed with the hysteresis loop squareness (R_{sq}), which can be calculated from the empirical expression $R_{sq} = (P_r/P_s) + (P_{1.1E_c}/P_s)$, where P_r is the remnant polarization, P_s is the saturated polarization obtained at some finite field strength below the dielectric breakdown and $P_{1.1E_c}$ is the polarization at the field equal to $1.1E_c$ [20]. For the ideal square loop, R_{sq} is equal to 2.00. As listed in Table 3, the R_{sq} parameter increases from 1.483 in $x = 0$ to reach the maximum value of 1.712 in $x = 0.3$. Further addition of MnO_2 above 0.3 wt% leads to a decrease in the R_{sq} parameter, which is mainly attributable to non-uniformity of the microstructure, as shown in Figure 2. The longitudinal strain (ϵ) of the specimens as a function of the electric field is shown in Figure 7. The strains are degraded markedly when MnO_2 content is increased, as listed in Table 3. These results (decreased P_r and strain level but increased E_c) clearly indicate the "hard" characteristics with addition of MnO_2 , mainly caused by Mn ions substitution in B-site leads to the creation of oxygen vacancies, which pin the movement of the ferroelectric domain walls.

4. CONCLUSIONS

The structure and electrical properties of MnO_2 -doped 0.2Pb $(\text{Zn}_{1/3}\text{Nb}_{2/3})\text{O}_3$ -0.8Pb $(\text{Zr}_{1/2}\text{Ti}_{1/2})\text{O}_3$ ceramic, which is the MPB composition of the PZN-PZT system, are investigated. The addition of MnO_2 content transforms the crystal structure to rhombohedral side. Furthermore, MnO_2 addition decreases the Curie temperature, ϵ_c , d_{33} and k_p , but enhances the mechanical quality factor. The $P-E$ and $r-E$ loops demonstrate decreased P_r and strain level with increased E_c with addition of MnO_2 . These results clearly show the hardening influence of MnO_2

in the PZN-PZT system.

5. ACKNOWLEDGEMENTS

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Effect of Vibro- Milling Time on Phase Formation and Particle Size of $ZnNb_2O_6$ Nano-powders

Athipong Ngamjarurojana^{1,*}, Rattikorn Yimnirun² and Supon Ananta¹

¹Department of Physics, Faculty of Science, Chiang Mai University, Chiang Mai 50200 Thailand

²School of Physics, Institute of Science, Suranaree University of Technology, Nakhon Ratchasima 30000 Thailand

Keywords: Zinc niobate; Vibro-milling; solid-state reaction; Microstructure; Dielectric Properties

ABSTRACT

Zinc niobate, $ZnNb_2O_6$, nanopowders was synthesized by a solid-state reaction via a rapid vibro-milling technique. The effect of milling time on the phase formation and particle size of $ZnNb_2O_6$ powder was investigated. The formation of the $ZnNb_2O_6$ phase investigated as a function of calcination conditions by DTA and XRD. The particle size distribution of the calcined powders was determined by laser diffraction technique, while morphology, crystal structure and phase composition were determined via a SEM techniques. In addition, by employing an appropriate choice of milling time, a narrow particle size distribution curve was also observed.

INTRODUCTION

Zinc niobate ($ZnNb_2O_6$, ZN) is one of the binary niobate compounds which exhibits excellent dielectric properties at microwave frequencies [1-2]. It has very low loss and high dielectric constant and is a promising candidate for application in microwave devices[3-4]. Moreover, the columbite-structured $ZnNb_2O_6$ is well known as an attractive B-site precursor for the preparation of lead zinc niobate ($Pb(Zn_{1/3}Nb_{2/3})O_3$ or PZN)-based ferroelectric ceramics used for high performance electromechanical actuators and transducers and piezoelectric ultrasonic motors [5-7]. This is significant because it is very difficult to synthesize those compounds via the conventional solid-state reaction process using oxides as starting materials [8-10]. In the past, $ZnNb_2O_6$ powders were usually prepared by a solid-state reaction process [11-13]. Recent work by Vittayakorn *et. al.* [14] has also shown promise in producing pure phase columbite ZN powders with the conventional mixed-oxide ball milling method technique that used very long heat treatments at ~950-1350 °C for 4h, while Ngamjarurojana *et. al.*[15] has successfully synthesized ZN powders via a rapid vibro-milling technique, which have been developed as alternatives to the conventional solid-state reaction of mixed oxides. These techniques are aimed at reducing the temperature of preparation of the compound by mixed oxide route.

Therefore, the main purpose of this work is to explore a simple mixed oxide synthetic route for the production of $ZnNb_2O_6$ (ZN) powders via a rapid vibro-milling technique and to perform milling time, which calcined at 600 °C for 2 h with heating/cooling rates 5 °C/min, on the phase formation and particle size of $ZnNb_2O_6$ powder was investigated.

EXPERIMENTAL

In this study, starting materials were commercially available zinc oxide, ZnO (Fluka Chemical, 99.9% purity) and niobium oxide, Nb_2O_5 (Aldrich, 99.9% purity). $ZnNb_2O_6$ powders were synthesized by the solid-state reaction of these raw materials. Ground mixtures of the powders were required with stoichiometric ratio of ZnO and Nb_2O_5 powders. A McCrone vibro-milling technique

was employed in order to combine mixing capacity with a significant time saving. The milling operation was carried out in isopropanol. High purity corundum cylindrical media were used as the milling media. After varied vibro-milling from 0.5- 25 h. and drying at 120 °C, the mixture was calcined at 600 °C for 2 h with heating/cooling rates 5 °C/min[13] in alumina crucible to investigate the phase formation behavior of ZN powders. Calcined powders were subsequently examined by room temperature X-ray diffraction (XRD; Siemens-D500 diffractometer) using Ni-filtered CuK α radiation to identify the phases formed for the ZN powders. Powder morphologies and particle sizes were directly imaged using scanning electron microscopy (SEM; JEOL JSM-840A). The particle size distributions of the powders were determined by laser diffraction technique (Zetasizer Nano; Malvern Particle Size).

RESULTS AND DISCUSSION

All calcined powders in together different vibro-milling time as shown in Fig. 1. It can be noticed that all conditions is pure phase of ZnNb₂O₆ which are matched in JCPDS file number 30-0873.

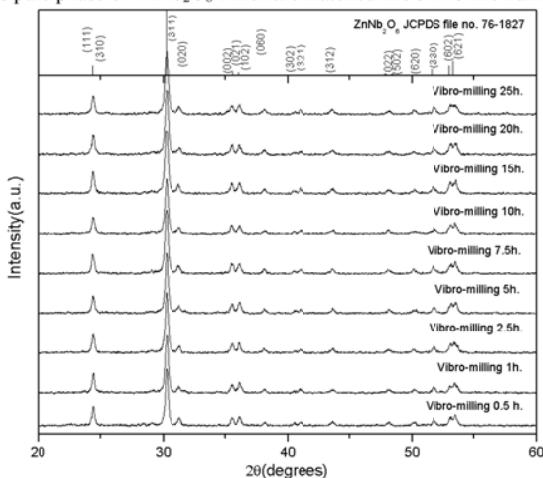


Fig. 1 XRD patterns of the ZN powders calcined at 600 °C for 2 h with heating/cooling rates 5 °C/min with various milling times.

Fig. 2 shows the morphological evolution of all samples as a function of milling times. In general, the particles are agglomerated and basically irregular in shape, with a substantial variation in particle sizes. By increasing the milling time from 0.5 h to 25 h, the particle size of the ZN powder almost similar in size and shape. This is probably due to the effectiveness of vibro-milling and carefully optimized reaction. It is also of interest to point out that larger particle size was obtained for the milling time longer than 10 h. This observation may be attribute to the occurrence of hard agglomeration with strong inter-particle bond within each aggregates resulting from high energy of too long milling time process.

The effect of milling time on particle size distribution was found to be quite significant as shown in Fig 3. After milling times of 0.5–7.5 h, the powders have similar particle size distribution behavior. They exhibit a single peak covering the size ranging from 0.3 – 0.8 μ m. By increasing the milling time to 10 h, a uniform particle size distribution with a much lower degree of particle agglomeration was found. However, upon further increasing of milling time up to 25h, a distribution curve with peak broadening between 0.2 – 1 μ m was observed. This may be attribute to

the formation of hard and large agglomeration found in the SEM results. In this work, it is seen that the optimum milling time for the production of smallest nanosized and high purity ZN powder was found to be at 10 h. Variations in these data may be attributed mainly to the formation of hard and large agglomerations found in the SEM results.

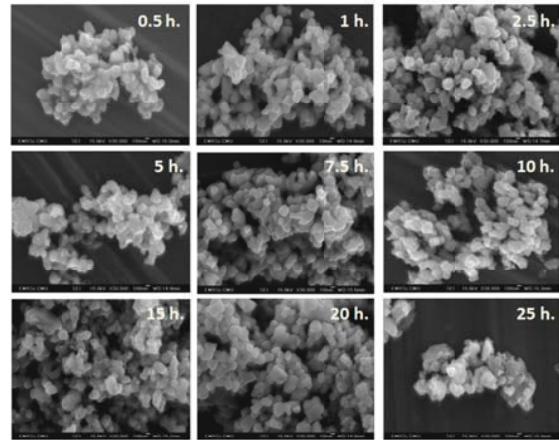


Fig. 2 SEM micrographs of the calcined ZN powders with various milling times.

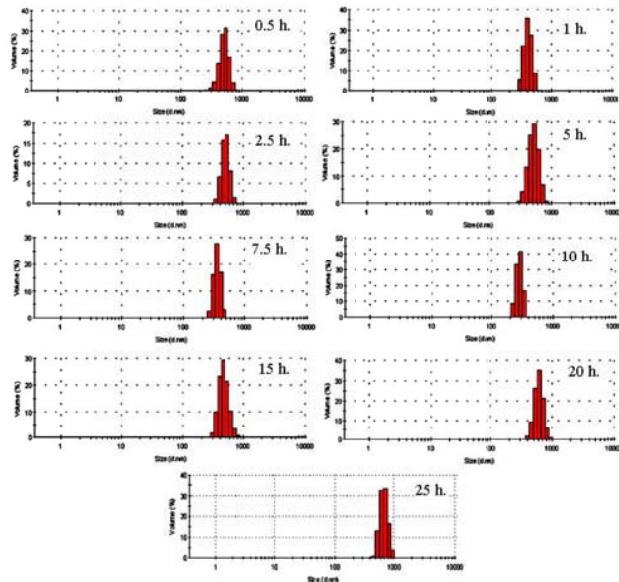


Fig. 3 Particle size distribution curves of the calcined ZN powders with various milling times.

CONCLUSIONS

The effect of milling times on phase formation, particle size and particle size distribution of perovskite zinc niobate synthesized by the solid-state reaction via a rapid vibro-milling technique was investigated. The resulting ZN nano-sized powders consist of a variety of agglomerate particle size, depending on milling times.

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e-mail: ngamjarurojana@yahoo.com

Fax: +66-53-943445

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Extended X-Ray Absorption Fine Structure and X-Ray Diffraction Studies of Mn-Doped PZN-PZT Ceramics

Athipong Ngamjarurojana, Laongnuan Srisombat, Rattikorn Yimmirun,
and Supon Ananta

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PZN-PZT Ceramics
Athipong Ngamjarurojana, Laongnuan Srisombat, Rattikorn Yimmirun,
and Supon Ananta

1 **Extended X-Ray Absorption Fine Structure and**
 2 **X-Ray Diffraction Studies of Mn-Doped PZN-PZT**
 3 **Ceramics**

4 ATHIPONG NGAMJARUROJANA,^{1,4}
 5 LAONGNUAN SRISOMBAT,² RATTIKORN YIMNIRUN,³
 6 AND SUPON ANANTA^{1,*}

7 ¹Department of Physics and Materials Science, Faculty of Science,
 8 Chiang Mai University, Chiang Mai 50200, Thailand

9 ²Department of Chemistry, Faculty of Science, Chiang Mai University,
 10 Chiang Mai 50200, Thailand

11 ³School of Physics, Suranaree University of Technology, Nakhon Ratchasima
 12 30000, Thailand

13 ⁴ThEP Center, CHE, 328 Si Ayutthaya Road, Bangkok 10400, Thailand

14 *In this work, the selected compositions of a combination between perovskite piezo-
 15 electric ceramics lead zinc niobate (PZN) and lead zirconate titanate (PZT), close to
 16 the morphotropic phase boundary (MPB) i.e. the 0.2PZN-0.8PZT, doped with MnO₂
 17 concentrations of 0.9–0.9 wt% were fabricated by a simple solid-state reaction and a
 18 pressureless sintering techniques. X-ray diffraction (XRD) spectra from these materi-
 19 als reveal transformation of the tetragonal into the rhombohedral structure. The local
 20 structure of Mn was analyzed by mean of synchrotron extended X-ray absorption fine
 21 structure (EXAFS) measurements at the Mn K-edge. The correlation between the struc-
 22 tural changes and the Mn content was analyzed and compared. The EXAFS analysis
 23 indicates that Mn ions should occupy the B-sites in PZN-PZT structure and plays a
 24 critical role for the hard ferroelectric behavior of the material.*

25 **Keywords** Piezoceramics; perovskite; EXAFS; X-ray diffraction

26 **1. Introduction**

27 Lead-based complex perovskite piezoceramics with general formula Pb(B',B'')O₃ such
 28 as PZN, PZT and their solid-solutions close to the MPB are very attractive for sensor,
 29 transducer and actuator applications [1–3]. This is because of their low firing temperature
 30 and excellent piezoelectric properties. It has been widely proposed that these important
 31 properties strongly depend on the rotations and distortions of the BO₆ octahedra [1, 2].
 32 Manganese oxide is one of the key effective dopants for lead-based perovskite piezoe-
 33 ramics to exhibit hard ferroelectric behavior [4–6]. Because of different valence of Mn and
 34 B-site ions, an enhancement in the Mn/B-site ions ratio may increase the vacancy concen-
 35 tration, forming acceptor-type defects and/or etc. In our previous work [7], the structure

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*Corresponding author. E-mail: suponananta@yahoo.com

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36 and electrical properties of MnO_2 -doped 0.2PZN-0.8PZT compositions were investigated.
 37 It was found that with the addition of MnO_2 , Curie temperature, the piezoelectric constant
 38 and electromechanical coupling factor were slightly decreased, but the mechanical quality
 39 factor was significantly enhanced. However, so far, the nature of the hard ferroelectric re-
 40 sponse and the site preference of Mn in these complex perovskite materials are still unclear
 41 [4–7]. Additionally, these previous investigation on Mn-doped PZT-based ceramics has
 42 also assumed that Mn ions sit in B-site [4–7]. Interestingly, so far, there has been no direct
 43 experimental determination of Mn-site in these materials. Thus, in this work, a combina-
 44 tion of X-ray diffraction (XRD) and synchrotron extended X-ray absorption fine structure
 45 (EXAFS) experiments [8, 9], which is proven to be a powerful technique for resolving the
 46 local structure surrounding a particular (absorbing) atom, was performed on the Mn-doped
 47 PZN-PZT system in order to determine the local structure around Mn ions.
 48

49 2. Experimental

50 The selected samples studied were fabricated according to the formula $0.2\text{Pb}(\text{Zn}_{1/3}\text{Nb}_{2/3})$
 51 $\text{O}_3.0.8\text{Pb}(\text{Zr}_{1/2}\text{Ti}_{1/2})\text{O}_3 + x \text{ wt\% MnO}_2$, where $x = 0.0$ to 0.9 by a simple mixed-oxide
 52 method as detail described elsewhere [7]. Starting materials of PbO , ZnO , Nb_2O_5 , ZrO_2 ,
 53 TiO_2 , and MnO_2 with >99% purity were vibro-milled with zirconia media in isopropanol
 54 for 30 min. After drying, the powders were calcined at 900°C for 2 h. The calcined PZN-
 55 PZT powders were vibro-milled with MnO_2 additive and PVA binder for 30 min, pressed
 56 into pellets and fired at 500°C for 1 h to eliminate the PVA, followed by sintering with PbO -
 57 rich atmosphere inside sealed alumina crucible at 1200°C for 2 h [7]. Phase identification
 58 of the samples was performed by XRD and densities were measured by Archimedes
 59 method. The synchrotron EXAFS measurement was performed in the transmission mode
 60 at the X-ray absorption spectroscopy beamline (BL-8) of the Siam photon source (electron
 61 energy of 1.2 GeV), Synchrotron Light Research Institute (Public Organization), Thailand
 62 (Fig. 1). The spectra were collected at ambient temperature with a Ge(111) double crystal

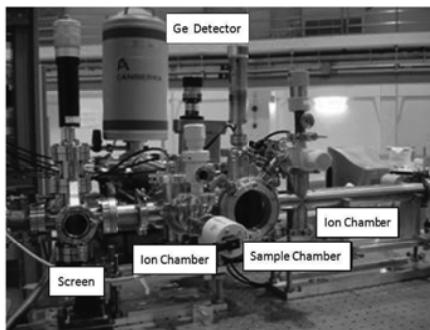


Figure 1. EXAFS experimental set-up at BL8, SPS.

63 monochromator and recorded after performing an energy calibration. To increase the count
64 rate, the ionization chamber was filled with Ar gas. The storage ring was running at an
65 energy of 1.2 GeV with electron currents between 80 mA and 30 mA.

66 3. Results and Discussion

67 The XRD patterns of $0.2\text{Pb}(\text{Zn}_{1/3}\text{Nb}_{2/3})\text{O}_3\text{-}0.8\text{Pb}(\text{Zr}_{0.52}\text{Ti}_{0.48})\text{O}_3$ ceramics at different Mn
68 concentrations are shown in Fig. 2. In general, the strongest reflections apparent in the
69 majority of these XRD patterns indicate the formation of the pure perovskite phase for
70 all compositions. It should be noted that no evidence of the pyrochlore-type compounds
71 [10, 11] was found in this study, nor was there any indication of the unreacted precursors
72 [12] being present. This is possibly due to uses of different processing methods. In those
73 either works, a conventional ball-milling was employed, while the rapid vibro-milling used
74 in this present study results in finer powders with apparently more reactivity, hence the
75 pure perovskite phase is formed more easily. Furthermore, the effective suppression of
76 PbO volatilization commonly found for lead-based perovskite ceramics during high firing
77 temperature [1, 2] was also achieved with the designed sample arrangement for the sintering
78 scheme [7]. The undoped PZN-PZT ceramics were characterized as tetragonal phase which
79 is indicated by the splitting of $(002)_T$ and $(200)_T$ peaks in the 2θ range from 43 to 45°, similar
80 to the reported by Hou *et al.* [13] and Yang *et al.* [14]. It is noticed that a small amount
81 of rhombohedral phase is also present with increasing Mn substitution with a complete
82 transformation to rhombohedral phase (revealed by the single $(202)_R$ peak) when x reaches
83 0.5 wt%. This is similar to the circumstance of PZN (rhombohedral phase) addition on
84 PZT system earlier reported by Lee *et al.* [11]. In addition, the effect of Mn on the shift
85 of MPB toward the rhombohedral phase region in the similar system of Mn-doped PZT
86 ceramics was also observed by Kim and Yoon [6]. It is believed that manganese ions are
87 mainly incorporated into the lattice, but if the addition is above 0.5 wt%, manganese ions
88 will accumulate at the grain boundaries [5]. It has been reported that manganese coexists
89 mainly in the Mn^{2+} and Mn^{3+} states, which entered into the perovskite structure of BO_6
90 octahedron to substitute for the B-site ion (e.g. Ti^{4+} and Zr^{4+}).

91 The MPB composition range has believed to be quite narrow, but in practice the MPB
92 has a wide range of compositions over which the tetragonal and rhombohedral phases
93 coexist in ceramics. Since all properties take extreme values near MPB, the width of the
94 MPB has been investigated by many workers and found to be related to the heterogeneous
95 distribution of Zr^{4+} and Ti^{4+} cations on the B-site of perovskite lattice [5, 6]. By means
96 of XRD, the co-existence of the two phases over a range of compositions around the MPB
97 was demonstrated in this work. The smaller ionic radius of Mn^{4+} ion (0.053 nm) compared
98 with that of the B-site ions (either Zn^{2+} (0.083 nm), Nb^{5+} (0.069 nm), Zr^{4+} (0.082 nm) or
99 Ti^{4+} (0.064 nm) [1, 15] leads to the reductions in the lattice constants (and tetragonality)
100 in Mn-doped PZN-PZT ceramics. However, the information on site preference of Mn in
101 PZN-PZT perovskite structure cannot be retrieved directly from the XRD analysis alone.
102 The EXAFS analysis was then employed to further study the local structure of Mn in the
103 PZN-PZT-based lattice.

104 Figure 3 show the Mn K edge and Fourier transforms for the EXAFS spectra with
105 possible bonding information identified and local structure of Mn-doped 0.2PZN-0.8PZT
106 ceramics. The Fourier transform is a complex function of distance R , the amplitude of
107 which is denoted by the real function $\rho(R)$. The position of peaks in $\rho(R)$ is related to
108 bond distances between the Mn ion and neighboring ions while the height of each peak
109 is proportional to the number of neighbors. The bond lengths and coordination numbers

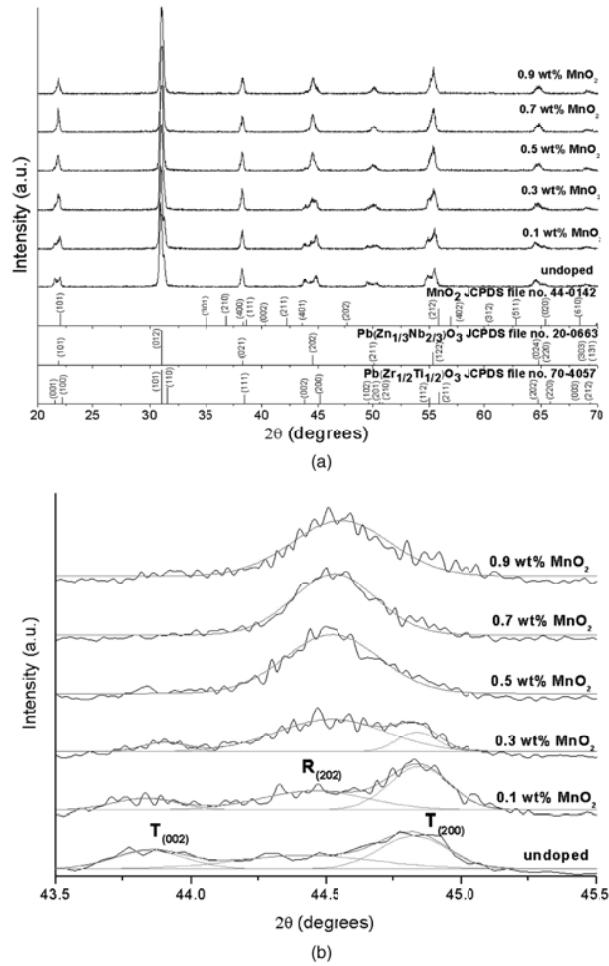


Figure 2. (a) XRD patterns of $0.2\text{Pb}(\text{Zn}_{1/3}\text{Nb}_{2/3})\text{O}_3 + 0.8\text{Pb}(\text{Zr}_{1/2}\text{Ti}_{1/2})\text{O}_3 + x \text{ wt\% MnO}_2$, where $x = 0.0$ to 0.9 and (b) enlarged XRD patterns in the $2\theta = 43\text{--}46^\circ$. (See Color Plate XXX)

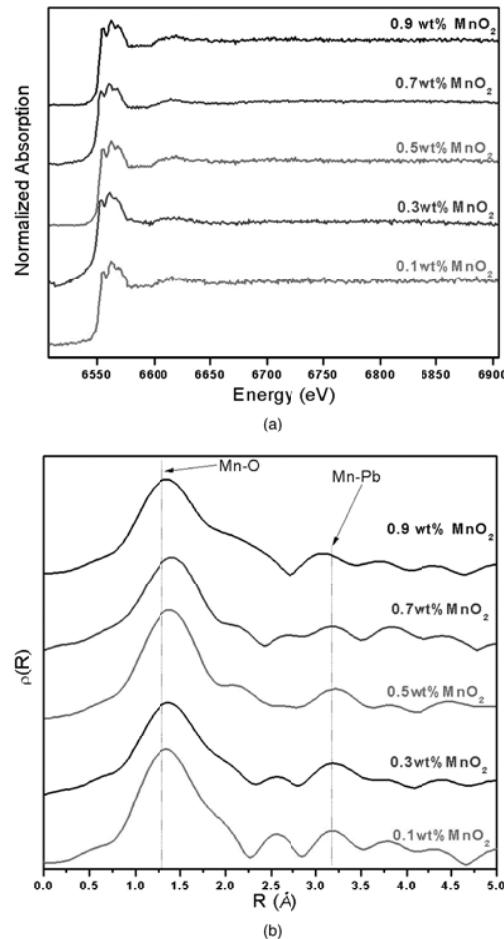


Figure 3. (a) Mn K edge spectra of MnO₂ doped 0.2PZN-0.8PZT ceramics, (b) Fourier transforms of the EXAFS spectra for MnO₂ doped 0.2PZN-0.8PZT ceramics (peaks are designed with possible bonding) and (c) Possible local structure for Mn-doped 0.2PZN-0.8PZT ceramics. (See Color Plate XXX)

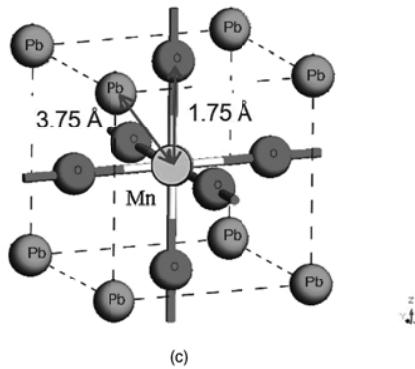


Figure 3. (Continued)

110 cannot, however, be read directly from $\rho(R)$. In order to determine the bond lengths and
 111 coordination numbers, the k -dependent amplitude and phase corrections must be made
 112 to the EXAFS signal. For example, prior to the phase correction, the peaks in $\rho(R)$ are
 113 basically smaller than the corresponding bond lengths by ~ 0.5 Å [9]. Interestingly, the
 114 location of Mn within PZN-PZT unit cell can be resolved without making phase and
 115 amplitude corrections. As shown in Fig. 3, by simply comparing the raw Fourier transform
 116 for different Mn contents (0.1–0.9 wt%), there is no observable change in peak positions,
 117 particularly for the first main peak. The coincidence of the main peaks is evidence that no
 118 change in the location of the majority of Mn ions occurs with increasing Mn concentration.
 119 Furthermore, the location of Mn appears to be unaffected by the presence of 0.9 wt%
 120 MnO_2 . It should be noted that a similar Fourier transform of EXAFS spectra for Mn doped
 121 PZN-PZT in this study, Mn doped PZT reported by Cherdhirunkorn *et al.* [9] and PZN,
 122 PZT perovskite established by Chen [16] is observed. The results indicate the site of Mn
 123 atom at B(Zn,Nb,Zr,Ti)-site in the PZN-PZT unit cell. Since the peak position indicates the
 124 bond distance between Mn and its neighbors or the location of Mn within the PZN-PZT unit
 125 cell, the unit cell of Mn-doped PZN-PZT can be extracted from the peak positions in the
 126 Fourier transform of EXAFS spectra shown in Fig. 3. According to the simulation EXAFS
 127 for Mn-doped PZT established by Cherdhirunkorn *et al.* [9], similar information can be
 128 extracted from the Fourier transforms of the EXAFS spectra from Mn-doped PZN-PZT
 129 observed in this work. It is very interesting to observe similar EXAFS signatures between
 130 the Mn-B-site curve where the first main peak occurring at ~ 1.25 Å (due to the six nearest
 131 oxygen atoms), while the second peak at ~ 3.2 Å is attributed to the nearest Pb atoms.
 132 Furthermore by comparing the results shown in Fig. 3 and Ref. [16], it is evident that the
 133 peaks are well consistent with a simulation of EXAFS that assumes Mn occupies the B-site
 134 but the minority A-site occupation cannot be ruled out.

135 **4. Conclusions**

136 A combination of X-ray diffraction and synchrotron extended X-ray absorption fine structure
 137 experiments is performed on Mn-doped $0.2\text{Pb}(\text{Zn}_{1/3}\text{Nb}_{2/3})\text{O}_3\text{-}0.8\text{Pb}(\text{Zr}_{1/2}\text{Ti}_{1/2})\text{O}_3$. The
 138 transformation of the tetragonal into the rhombohedral structure with increasing Mn content
 139 was revealed by XRD technique. The EXAFS analysis indicates that Mn ions should
 140 occupy the B(Zn, Nb, Zr, Ti)-sites in PZN-PZT structure and plays a critical role for the
 141 hard ferroelectric behavior of the materials.

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